

# UNCLASSIFIED

AD NUMBER
AD531281
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution limited to U.S. Gov't. agencies only; Test and Evaluation; Jul 74. Other requests for this document must be referred to Director, Naval Research Lab., Washington, D. C. 20375.
AUTHORITY
NRL ltr, 1 Jul 2002

THIS PAGE IS UNCLASSIFIED

UNCLASSIFIED



AD NUMBER

0531 281

CLASSIFICATION CHANGES

TO

UNCLASSIFIED

FROM

SECRET

AUTHORITY

31 DEC 89, IAW OCA MRKNGS ON DOC

Reproduced From  
Best Available Copy

THIS PAGE IS UNCLASSIFIED

**SECRET**

NRL Report 7765  
Copy No. ~~186~~

# Probability of Detecting Ships With an OTH Radar System

[Unclassified Title]

JON DAVID WILSON

*Radar Analysis Staff  
Radar Division*

July 10, 1974

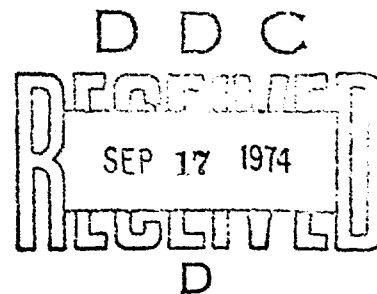
**Reproduced From  
Best Available Copy**

"NATIONAL SECURITY INFORMATION"

"Unauthorized Disclosure Subject to Criminal  
Sanctions"



**NAVAL RESEARCH LABORATORY  
Washington, D.C.**



**DDC CONTROL  
NO 42495**

**SECRET**

SECRET, classified by CNO msg 021634Z, June 1971.  
Exempt from GDS of E.O. 11652 by CNO msg 021634Z.  
Ex. Cat. (3). Auto. declass. on Dec. 31, 1989.

## **REPRODUCTION QUALITY NOTICE**

**This document is the best quality available. The copy furnished to DTIC contained pages that may have the following quality problems:**

- **Pages smaller or larger than normal.**
- **Pages with background color or light colored printing.**
- **Pages with small type or poor printing; and or**
- **Pages with continuous tone material or color photographs.**

**Due to various output media available these conditions may or may not cause poor legibility in the microfiche or hardcopy output you receive.**

☐ **If this block is checked, the copy furnished to DTIC contained pages with color printing, that when reproduced in Black and White, may change detail of the original copy.**

**SECRET**

**NATIONAL SECURITY INFORMATION**

Unauthorized Disclosure Subject to Criminal Sanctions.

**Reproduced From  
Best Available Copy**

**SECRET**

**SECRET**

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NRL Report 7765	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) PROBABILITY OF DETECTING SHIPS WITH AN OTH RADAR SYSTEM [Unclassified Title]		5. TYPE OF REPORT & PERIOD COVERED This is an interim report; work is continuing
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Jon David Wilson		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Research Laboratory Washington, D.C. 20375		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS R02-46A WF 12-111-704
11. CONTROLLING OFFICE NAME AND ADDRESS Department of the Navy Naval Air Systems Command Washington, D.C. 20361		12. REPORT DATE July 10, 1974
		13. NUMBER OF PAGES 46
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) SECRET
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE XGDS (3) - 1989
16. DISTRIBUTION STATEMENT (of this Report) Distribution limited to U.S. Government Agencies only; test and evaluation; July 1974. Other requests for this document must be referred to the Director, Naval Research Laboratory, Washington, D.C. 20375.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Over-the-horizon radar Probability of ships detection Probability of skywave propagation Sea clutter spectrum		<div style="text-align: center;"> D D C  RECEIVED  SEP 17 1974  REGULATED  D </div>
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) (U) An over-the-horizon (OTH) radar uses ionospheric reflection of high-frequency radio waves to propagate to areas far beyond the normal radar horizon. Two principle probabilities are associated with an OTH radar: the probability of successfully propagating to a given region via the ionosphere and the probability of detecting a target in sea clutter, given that propagation occurred. A particular radar system was examined and tables of probabilities were generated for various ionospheric and target parameters. An example illustrates the method of combining these probabilities to obtain a composite probability of (Continued)		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE  
S/N 0102-014-6601

**SECRET**

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

**20. Abstract (Continued)**

detection. The probability of propagating was calculated by a computer program that used radar parameters, the ionospheric parameters, the geographical location, and the time of day and year as inputs. The probability of detection involved a computer implementation of the radar range equation.

SECRET

## CONTENTS

INTRODUCTION .....	1
PROBABILITY OF PROPAGATION .....	1
PROBABILITY OF DETECTION .....	15
RESULTS .....	17
ACKNOWLEDGMENTS .....	43
REFERENCES .....	43

SEP 17 1976  
RECEIVED  
DDC CONTROL  
NO 42488



SECRET

## PROBABILITY OF DETECTING SHIPS WITH AN OTH RADAR SYSTEM [Unclassified Title]

### INTRODUCTION

(U) This report is based on one phase of a study being conducted at the Naval Research Laboratory (NRL) [1-6] to compare the cost and effectiveness of three different radar systems used for ocean surveillance. The three candidate systems are an airborne radar, a satellite-borne radar, and a ground-based over-the-horizon (OTH) radar. For this report, the probability of detection of one particular OTH system has been calculated. The methods used, however, can be applied to any OTH system.

### PROBABILITY OF PROPAGATION

(S) The ability of a radar system to propagate to a given range at a given time of the year was found by using RADARC, which is a computer program written by the Institute of Telecommunication Sciences to meet OTH radar analysis requirements as specified by NRL [7]. This program calculates the median clutter-to-noise ratio (C/N) for an OTH radar. The size of the backscatter area is calculated from virtual height ionograms using geometrical optics techniques. The noise considered includes atmospheric, galactic, and man-made sources. Atmospheric and ionospheric losses are included and the C/N is calculated from the radar range equation. This calculation was performed for sporadic  $E$ ,  $E$ ,  $F_1$ , and  $F_2$  layer propagation modes. If the clutter return and signal return are assumed to be affected by the ionosphere in a similar manner, propagation is defined by requiring the signal return from 1000-m<sup>2</sup> target to be large enough against noise to yield a probability of detection  $P_D$  equal to 0.9 and a probability of false alarm  $P_{fa}$  equal to  $10^{-6}$  for a Type 1 OTH FM-CW radar system [6]. This system has the following parameters:

- 100-kw average power
- 0.1-s frequency sweep (prf = 10 per second)
- 20- $\mu$ s compressed pulse length
- 2.5-km horizontal aperture, receive ( $\approx 0.25^\circ - 1^\circ$ ), transmit ( $\approx 6^\circ - 10^\circ$ ).

We now calculate the C/N required for propagation.

(S) First, in order to obtain a  $P_{fa} = 10^{-6}$  and a  $P_D = 0.9$ , the integrated signal-to-noise ratio (S/N) should be 13 dB. The FM-CW radar system is assumed to have 10 frequency sweeps per second, a coherent integration time of 25 s, and a total integration time of 250 s. From Rubin and Difranco [8], the noncoherent integration gain for 10 noncoherent pulses is found to be 7 dB. With coherent integration, the noise spectrum extends from -5 to +5 Hz and is separated into 250 doppler bins of width 0.04 Hz. Thus,

---

Note: Manuscript submitted May 14, 1974.

the required  $S/N$  per doppler bin is 6 dB, (13 dB - 7 dB), and the  $S/N$  in a cycle bandwidth is -8 dB, or [6 dB + 10 log (0.04)]. Since the signal and clutter are assumed to propagate in a similar manner, the signal-to-clutter ratio ( $S/C$ ) is given by

$$\frac{S}{C} = \frac{\sigma_T}{\frac{\sigma_0 \theta_B R c \tau}{2}} = -33 \text{ dB} \quad (1)$$

where

- $\sigma_T$  = target cross section (30 dBsm),
- $\sigma_0$  = relative sea clutter cross section (-17 dB)
- $\theta_B$  = antenna beamwidth ( $1^\circ$ )
- $R$  = radar range, 1000 n.mi.
- $c$  = speed of light
- $\tau$  = effective pulse width, 20  $\mu$ s.

Now, the required  $C/N$  for propagation is calculated from

$$\frac{C}{N} = \frac{\frac{S}{N}}{\frac{S}{C}} = 25 \text{ dB.}^* \quad (2)$$

Even though the main antenna pattern is wired into RADARC, the received clutter and noise powers are independent of the receive antenna beamwidth,† and consequently, RADARC can be used to calculate propagation for the FM-CW radar system. The only alterations made to the program were to eliminate printed output and to add the punched output used in calculating the propagation statistics.

(S) The ability to propagate was found for four months, (January, April, July, or October), two times (day or night), and three sunspot numbers (20, 45, or 75, which are the 25th, 50th, and 75th percentiles). The radar is situated in Maine (latitude  $45^\circ$  N, longitude  $67^\circ$  W). For each of the 24 conditions, the radar model RADARC was used to calculate the  $C/N$  every 2 hr for three azimuth angles ( $14^\circ$ ,  $59^\circ$ , and  $104^\circ$ ), spanning a  $90^\circ$  sector. For each set of parameters, one-bounce propagation via four layers (sporadic E, E,  $F_1$ ,  $F_2$ ) was considered and the maximum  $C/N$  chosen. The number of occasions out of 18 (6 times, 2 hr apart, and 3 azimuths) that the  $C/N$  exceeded 25 dB is given in Tables 1-24. We can interpret these numbers divided by 18 as a probability of propagation. If

\*Specifically, a  $C/N$  of 25 dB is equivalent to our defined propagation at 1000 n.mi. for a 30-dB target and the particular frequency that yields a  $1^\circ$  beamwidth. For other ranges, targets, and frequencies, 25 dB was still used since  $C/N$  varies rapidly with range and hence a change in the threshold (25 dB) would have little effect on the region of propagation.

†When the transmit beamwidth is larger than the receive beamwidth, the receive array is sampling an extended source. When the beamwidth narrows, the clutter (or atmospheric noise) patch narrows, but the gain of the array increases.

SECRET

NRL REPORT 7765

(U) Table 1  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in nighttime with SNS=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = JAN		NIGHT		SUN SPOT = 20			
	6	9	12	15	18	21	24	27
500	16	13	9	0	0	0	0	0
1000	18	16	13	10	7	3	0	0
1500	17	2	0	0	0	0	0	0
2000	15	5	0	0	0	0	0	0

(U) Table 2  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in daytime with SSN=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = JAN		DAY		SUN SPOT = 20			
	6	9	12	15	18	21	24	27
500	18	18	9	0	0	0	0	0
1000	16	18	18	14	4	0	0	0
1500	3	9	13	12	8	3	0	0
2000	2	4	4	5	5	5	0	0

(U) Table 3  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in nighttime with SSN=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = APR NIGHT SUN SPOT = 20							
	6	9	12	15	18	21	24	27
500	18	12	6	0	0	0	0	0
1000	18	16	12	8	3	0	0	0
1500	15	8	4	0	0	0	0	0
2000	12	10	5	1	0	0	0	0

(U) Table 4  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in daytime with SSN=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = APR DAY SUN SPOT = 20							
	6	9	12	15	18	21	24	27
500	18	18	4	0	0	0	0	0
1000	8	16	15	11	2	0	0	0
1500	0	4	9	10	1	0	0	0
2000	0	2	5	7	5	0	0	0

SECRET

NRL REPORT 7765

(U) Table 5  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in nighttime with SSN=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = JUL		NIGHT		SUN SPOT = 20			
	6	9	12	15	18	21	24	27
500	18	18	15	4	3	0	0	0
1000	18	18	18	17	15	8	5	2
1500	13	11	6	1	0	0	0	0
2000	7	11	6	3	0	0	0	0

(U) Table 6  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in daytime with SSN=20  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = JUL		DAY		SUN SPOT = 20			
	6	9	12	15	18	21	24	27
500	17	16	16	2	1	0	0	0
1000	5	13	17	10	13	13	6	1
1500	0	3	9	8	0	0	0	0
2000	0	1	2	3	3	0	0	0

(U) Table 7  
 Number of successful propagations out of 18 possible opportunities, in October, in nighttime with SSN=20 as a function of range and frequency

	MONTH = OCT		NIGHT		SUN SPOT =	20		
					FREQUENCY (MHZ)			
	6	9	12	15	18	21	24	27
RANGE (NM)	.....							
500	18	15	9	2	0	0	0	0
1000	18	18	15	12	8	4	2	0
1500	16	7	1	0	0	0	0	0
2000	14	10	1	0	0	0	0	0

(U) Table 8  
 Number of successful propagations out of 18 possible opportunities, in October, in daytime with SSN=20 as a function of range and frequency

	MONTH = OCT		DAY		SUN SPOT =	20		
					FREQUENCY (MHZ)			
	6	9	12	15	18	21	24	27
RANGE (NM)	.....							
500	18	18	9	0	0	0	0	0
1000	11	18	18	17	6	2	0	0
1500	3	7	14	15	8	2	0	0
2000	0	4	6	9	13	7	0	0

SECRET

NRL REPORT 7765

(U) Table 9  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in nighttime with SSN=45  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	NIGHT				SUN SPOT = 45			
	6	9	12	15	18	21	24	27
500	16	13	8	0	0	0	0	0
1000	18	16	13	9	5	3	0	0
1500	17	5	0	0	0	0	0	0
2000	15	11	0	0	0	0	0	0

(U) Table 10  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in daytime with SSN=45  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	DAY				SUN SPOT = 45			
	6	9	12	15	18	21	24	27
500	18	18	13	0	0	0	0	0
1000	15	18	18	16	7	0	0	0
1500	3	8	15	14	11	7	2	0
2000	1	6	9	5	8	7	5	0

SECRET

(U) Table 11  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in nighttime with SSN=45  
 as a function of range and frequency

RANGE (NM)	MONTH = APR		NIGHT		SUN SPOT = 45			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
500	18	13	5	6	0	0	0	0
1000	18	17	14	8	3	0	0	0
1500	14	14	5	2	0	0	0	0
2000	12	13	8	4	0	0	0	0

(U) Table 12  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in daytime with SSN=45  
 as a function of range and frequency

RANGE (NM)	MONTH = APR		DAY		SUN SPOT Δ		45	
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
500	17	18	3	0	0	0	0	0
1000	5	13	18	9	2	0	0	0
1500	0	3	8	12	7	0	0	0
2000	0	2	5	6	8	4	0	0



SECRET

NRL REPORT 7765

(U) Table 13  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in nighttime with SSN=45  
 as a function of range and frequency

	MONTH = JUL		NIGHT		SUN SPOT = 45			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
*****								
RANGE (NM)								
500	18	18	15	3	2	0	0	0
1000	18	18	18	16	14	8	5	2
1500	12	15	7	3	0	0	0	0
2000	6	14	6	6	1	0	0	0

(U) Table 14  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in daytime with SSN=45  
 as a function of range and frequency

	MONTH = JUL		DAY		SUN SPOT = 45			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
*****								
RANGE (NM)								
500	16	18	15	2	1	0	0	0
1000	5	11	17	8	13	13	6	1
1500	0	2	6	13	1	0	0	0
2000	0	0	2	2	8	0	0	0

(U) Table 15  
 Number of successful propagations out of 18 possible  
 opportunities, in October, in nighttime with SSN=45  
 as a function of range and frequency

RANGE (NM)	MONTH = OCT		NIGHT		SUN SPOT = 45			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
♦♦								

(U) Table 16  
 Number of successful propagations out of 18 possible  
 opportunities, in October, in daytime with SSN=45  
 as a function of range and frequency

RANGE (NM)	MONTH = OCT		DAY		SUN SPOT = 45			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
♦♦♦								

SECRET

NRL REPORT 7765

(U) Table 17  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in nighttime with SSN=75  
 as a function of range and frequency

RANGE (NM)	MONTH = JAN		NIGHT		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
*****								
500	16	13	8	0	0	0	0	0
1000	18	15	13	9	4	1	0	0
1500	18	10	1	0	0	0	0	0
2000	15	14	2	0	0	0	0	0

(U) Table 18  
 Number of successful propagations out of 18 possible  
 opportunities, in January, in daytime with SSN=75  
 as a function of range and frequency

RANGE (NM)	MONTH = JAN		DAY		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
.....								
500	18	18	12	2	0	0	0	0
1000	2	18	18	16	9	4	0	0
1500	3	7	13	16	13	10	5	2
2000	2	4	7	12	10	10	7	5

(U) Table 19  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in nighttime with SSN=75  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = APR		NIGHT		SUN SPOT = 75			
	6	9	12	15	18	21	24	27
500	18	14	5	0	0	0	0	0
1000	18	18	14	8	3	0	0	0
1500	15	18	11	4	0	0	0	0
2000	11	15	14	6	2	0	0	0

(U) Table 20  
 Number of successful propagations out of 18 possible  
 opportunities, in April, in daytime with SSN=75  
 as a function of range and frequency

RANGE (NM)	FREQUENCY (MHZ)							
	MONTH = APR		DAY		SUN SPOT = 75			
	6	9	12	15	18	21	24	27
500	16	18	7	0	0	0	0	0
1000	5	14	18	14	4	0	0	0
1500	0	3	7	12	11	5	0	0
2000	0	2	4	7	11	10	3	0

SECRET

NRL REPORT 7765

(U) Table 21  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in nighttime with SSN=75  
 as a function of range and frequency

	MONTH = JUL		NIGHT		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
*****								
RANGE (NM)								
500	18	18	14	3	1	0	0	0
1000	18	18	18	15	14	7	5	1
1500	12	15	10	6	1	0	0	0
2000	6	14	13	7	4	0	0	0

(U) Table 22  
 Number of successful propagations out of 18 possible  
 opportunities, in July, in daytime with SSN=75  
 as a function of range and frequency

	MONTH = JUL		DAY		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
*****								
RANGE (NM)								
500	14	18	17	1	1	0	0	0
1000	2	10	18	9	17	16	5	1
1500	0	2	5	13	4	0	0	0
2000	0	0	2	3	7	1	0	0

(U) Table 23  
 Number of successful propagations out of 18 possible  
 opportunities, in October, in nighttime with SSN=75  
 as a function of range and frequency

RANGE (NM)	MONTH = OCT		NIGHT		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
+ +								

(U) Table 24  
 Number of successful propagations out of 18 possible  
 opportunities, in October, in daytime with SSN=75  
 as a function of range and frequency

RANGE (NM)	MONTH = OCT		DAY		SUN SPOT = 75			
	FREQUENCY (MHZ)							
	6	9	12	15	18	21	24	27
	♦♦♦							

the tables are compared, the following general conclusions can be reached about propagation when using the optimal frequency for a given range:

- Better at night than during the day
- Better in winter than in summer
- For the sunspot numbers considered, better for the higher sunspot numbers
- Propagation is very close to 100% for the shorter ranges.

The following conclusions can be reached about frequency preferences:

- Higher frequencies during daytime
- Higher frequencies during summertime
- Higher frequencies for higher sunspot numbers
- Higher frequencies for longer ranges.

## PROBABILITY OF DETECTION

(U) In the previous section successful propagation was defined in terms of detection of targets against noise. Consequently, in this section we will consider only the detection of targets in sea clutter.

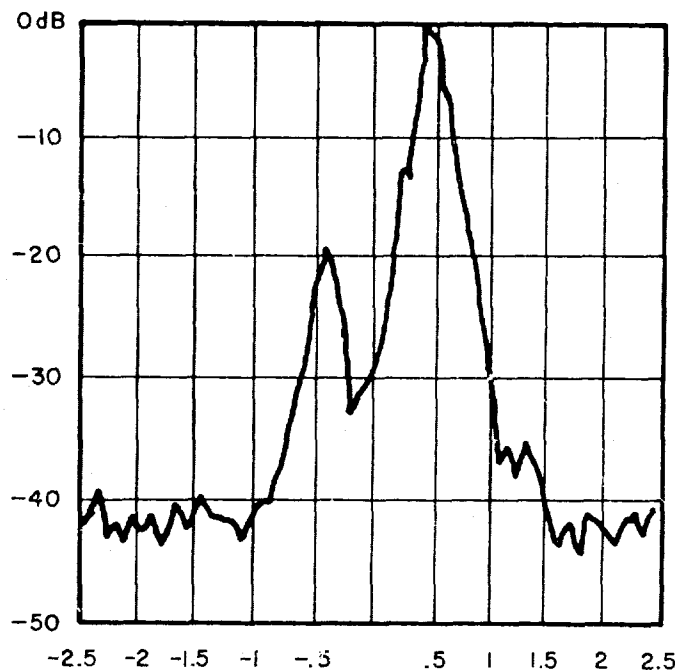
(C) The basic assumption is that the target return (small region) and the clutter return (extended region) will be affected in the same way by passage through the ionosphere. This allows us to calculate the  $S/C$  at the input to the processor from the target and clutter radar cross sections. The principal signal enhancement is from doppler processing with an additional noncoherent integration of the doppler cells.

(S) The  $S/C$  was calculated from Eq. (1) with three different target cross sections, 1000-m<sup>2</sup> and 3000-m<sup>2</sup> destroyers and a 50,000-m<sup>2</sup> aircraft carrier; and four ranges, 500, 1000, 1500, and 2000 n.mi, for each target type. The doppler processing gain was calculated for a set of radial velocities from -30 to +30 knots and a range of operating frequencies from 5 to 30 MHz. We assumed the target to be in one doppler cell and a 2-dB loss for processing and target doppler spread. The clutter level in a given doppler cell was obtained by normalizing a sample clutter spectrum. Two sample clutter spectra were derived from a working paper by Dr. James R. Barnum of Stanford Research Institute [9]. One asymmetrical spectrum represents the type of clutter spectrum observed with approaching (or receding) winds. The other spectrum is symmetric and is typical of the spectra observed in crosswind conditions.

(U) One observed clutter spectrum was used to generate both spectra. This particular spectrum was chosen on the basis of its clean appearance, but all of the candidate spectra from Ref. 9 have certain features in common, such as the Bragg scatter peaks, the lowered level of clutter between these peaks, and the even lower level of clutter in the doppler cells outside of the peak. The symmetrical (crosswind) clutter spectrum was obtained by averaging the clutter cells symmetrically placed about the carrier frequency. This process yielded a spectrum that appears to be a valid approximation to observed

crosswind spectra. This approximation was used because there was always at least a small asymmetry in the levels of the approaching and receding Bragg scattering lines of the observed spectra (an asymmetry would favor either the approaching or receding targets).

(U) The asymmetrical clutter spectrum is shown in Fig. 1. This spectrum was extended to  $\pm 5$  Hz at a -42 dB level. The sea clutter, of course, does not have a plateau at some particular level below the Bragg line peak but has been measured on the Madre radar (with a 70-dB dynamic range) to drop off to at least 65 to 70 dB below the peak at  $\pm 5$  Hz. The -42 dB plateau seems to be a feature of the radar on which the spectrum was measured. This would make little difference in our results: If the target is not in a Bragg line peak, it is detected. The two large spikes correspond to the Bragg scatter of ocean waves. The relative amplitude of the two spikes is a function of the angle of the ocean wavefront to the radar wavefront and hence depends on local wind direction [10]. The doppler offset of these spikes from the carrier frequency depends on the carrier frequency. The particular spectrum shown as measured at 20 MHz. At other radar frequencies, the spectral line spacing expands and contracts with the square root of the carrier frequency [11].



(U) Fig. 1—Typical clutter doppler spectrum

(S) The doppler cell in which the target appears is calculated from the radial speed  $V_r$  and operating wavelength  $\lambda$  by

$$\text{Doppler cell} = \frac{2V_r}{\lambda(0.04)} \quad (3)$$



(S) The clutter energy in that cell is calculated from the normalized clutter spectrum (shifted by the operating frequency). The  $S/C$  obtained for this radial speed and operating frequency combination is interpolated into a table of values, giving the  $P_d$  for 10 pulses [8]. For purposes of display, an array of symbols indicating the probability level for each combination of speed and frequency is printed. The  $P_d$  results for the approaching wind clutter spectrum are given in Figs. 2-13 and the crosswind results are given in Figs. 14-25. In the figures, an integer  $N$  indicates that  $P_d$  is between  $0.1(N)$  and  $0.1(N + 1)$  and a blank indicates that  $P_d$  is less than 0.1. The following observations can be made.

- Smaller targets can be detected only at the higher radial velocities, whereas the largest target can be detected in all doppler cells except those occupied by the Bragg scatter lines.
- Better detection performance is observed in the nonsymmetrical spectrum. This can be attributed (a) to the concentration of clutter energy in the larger Bragg scatter peak where detection is impossible in any case, and (b) to the consequent reduction of clutter energy in the remaining doppler cells.
- Targets can be detected in more of the doppler cells at higher frequencies. This is because the target doppler is proportional to frequency, whereas the clutter spectrum expands as the square root of the frequency. Thus, as the frequency is raised targets obscured by the clutter peak move into doppler cells of lower clutter.

(U) This last point may be the result of using one clutter spectrum taken at one carrier frequency and expanded and contracted for other frequencies. The clutter spectrum is affected by both sea state and frequency, but we did not have available sufficient data to make quantitative adjustment to the assumed spectrum. The doppler level in the cells away from the Bragg lines increases with the carrier frequency, and our sample spectrum was measured at a relatively high frequency. This means that at low frequencies the clutter levels used in our calculation are too high, but again, it would not affect our results; if a target is not in a Bragg line peak, it is detected.

(U) The preceding detection curves (Figs. 2-25) were based on the assumption that  $\sigma_0 = -17$  dB. However, since there is some controversy over the value of  $\sigma_0$  (Barnum has data that indicate  $\sigma_0 = -23$  dB [12]), additional detection curves are generated for  $\sigma_0 = -23$  dB. These curves are displayed in Figs. 26-49. Obviously the only difference between the results and the previous results is an improvement of 6 dB.

## RESULTS

(S) To obtain a composite  $P_d$ , we multiply the probability of propagation (from Tables 1-24) by the probability of detection given that propagation is successful (Figs. 2-49). Two examples, one for  $\sigma_0 = -17$  dB the other for  $\sigma_0 = -23$  dB, are shown in Figs. 50 and 51, respectively. The composite  $P_d$  for each of four ranges is plotted vs radial speed. The target has a 3000-m<sup>2</sup> radar cross section in April, in daytime under crosswind conditions, with a sunspot number of 45. The operating frequency for each range is the frequency that yields the best composite  $P_d$  over the largest speed range. Only closing speeds are shown because of the symmetrical clutter spectrum. From these curves it appears that it is very difficult to detect a 3000-m<sup>2</sup> target at radial speeds below 15 knots if  $\sigma_0 = -17$  dB and

		RADIAL SPEED (KNOTS)												
		-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99999999961						13321							3
6	99999999982						25421						1599	
7	999999999994						137542						279999	
8	9999999999961						158753						38999999	
9	99999999999971						29865						59999999	
10	99999999999982						379761						1699999999	
11	99999999999993						1489871						1799999999	
12	999999999999984						599982						2899999999	
13	999999999999995						299982						3899999999	
14	9999999999999991						399993						4999999999	
15	9999999999999996						499994						5999999999	
16	99999999999999971						48999						1999999999	
17	99999999999999992						59999						6999999999	
18	99999999999999998						199991						1799999999	
19	999999999999999999						199991						2999999999	
20	9999999999999999994						299991						8999999999	
21	9999999999999999994						299991						3999999999	
22	9999999999999999995						399992						3999999999	
23	9999999999999999999						389992						9999999999	
24	99999999999999999991						99993						4999999999	
25	99999999999999999991						99993						5999999999	
26	99999999999999999996						99993						1599999999	
27	99999999999999999997						99994						1999999999	
28	99999999999999999997						199994						1999999999	
29	99999999999999999998						199995						6999999999	
30	99999999999999999992						199995						7999999999	

(S) Fig. 2— $P_d$  of  $1000\text{-m}^2$  target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17\text{ dB}$

		RADIAL SPEED (KNOTS)												
		-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	9999999994													
6	999999999961													27
7	9999999999982													4999
8	99999999999994						1						1699999	
9	99999999999995						21						29999999	
10	9999999999999961						121						89999999	
11	9999999999999997						1411						1999999999	
12	99999999999999982						2521						1999999999	
13	999999999999999999						3631						1699999999	
14	999999999999999994						4742						7999999999	
15	999999999999999995						4743						3999999999	
16	9999999999999999991						1873						3899999999	
17	9999999999999999996						2974						4999999999	
18	99999999999999999971						2985						9999999999	
19	99999999999999999992						3985						5999999999	
20	99999999999999999992						3996						1999999999	
21	99999999999999999998						4896						6999999999	
22	99999999999999999999						4897						7999999999	
23	999999999999999999994						1997						2999999999	
24	999999999999999999994						2998						2999999999	
25	999999999999999999995						2998						8999999999	
26	999999999999999999999						2999						9999999999	
27	9999999999999999999981						3999						4999999999	
28	9999999999999999999981						3999						4999999999	
29	9999999999999999999991						3999						9999999999	
30	9999999999999999999996						4999						9999999999	

(S) Fig. 3 —  $P_d$  of  $1000\text{-m}^2$  target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -17\text{ dB}$

SECRET

NRL REPORT 7765

RADIAL SPEED(KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	9999999751												
6	9999999972												3
7	99999999983												1567
8	999999999995												168998
9	99999999999961												7999999
10	99999999999972												489999999
11	999999999999983						1						599999999
12	999999999999994						1						699999999
13	999999999999995						2						299999999
14	9999999999999951						2						279999999
15	9999999999999991						131						899999999
16	9999999999999997						42						499999999
17	99999999999999972						531						199999999
18	99999999999999992						541						599999999
19	99999999999999998						641						199999999
20	99999999999999999						652						699999999
21	999999999999999994						1452						279999999
22	999999999999999995						1463						399999999
23	999999999999999999						563						899999999
24	9999999999999999991						574						899999999
25	9999999999999999991						574						499999999
26	9999999999999999996						674						499999999
27	9999999999999999997						685						999999999
28	9999999999999999997						785						199999999
29	9999999999999999999						796						699999999
30	9999999999999999999						1796						699999999

(S) Fig. 4— $P_d$  of 1000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

RADIAL SPEED(KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999986642												
6	99999999663												1
7	999999999751												234
8	9999999999992												35675
9	99999999999993												4678867
10	999999999999994												157897689
11	9999999999999951												2689987999
12	9999999999999991												2799999999
13	99999999999999972												8999999999
14	99999999999999992						1						1499999999
15	99999999999999998						1						5999999999
16	999999999999999994						1						1999999999
17	999999999999999994						21						6999999999
18	9999999999999999991						21						2999999999
19	9999999999999999996						31						7999999999
20	9999999999999999996						32						3899999999
21	9999999999999999991						12						4999999999
22	9999999999999999992						131						1999999999
23	9999999999999999998						231						5999999999
24	9999999999999999998						241						5999999999
25	9999999999999999998						241						1999999999
26	9999999999999999999						352						2999999999
27	9999999999999999994						352						6999999999
28	9999999999999999994						452						7999999999
29	9999999999999999999						462						2999999999
30	9999999999999999999						463						3999999999

(S) Fig. 5— $P_d$  of 1000-m<sup>2</sup> target at 2000-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

## RADIAL SPEED (KNOTS)

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	9999999999661	489999994	599
6	9999999999982	169999961	1179999
7	9999999999994	279999971	38999999
8	99999999999961	49999993	499999999
9	99999999999971	59999994	1599999999
10	99999999999992	169999995	17999999999
11	99999999999993	29999991	27999999999
12	999999999999941	28999991	89999999999
13	999999999999991	39999992	49999999999
14	9999999999999961	99999992	59999999999
15	9999999999999962	99999993	15999999999
16	99999999999999931	16999994	19999999999
17	99999999999999982	16999994	27999999999
18	999999999999999821	79999995	29999999999
19	999999999999999851	79999996	89999999999
20	999999999999999862	29999996	48999999999
21	999999999999999864	39999991	49999999999
22	999999999999999895	39999991	19999999999
23	999999999999999898	49999991	19999999999
24	9999999999999998964	99999991	69999999999
25	9999999999999998984	99999992	69999999999
26	9999999999999998984	99999992	29999999999
27	9999999999999998984	99999992	29999999999
28	9999999999999998984	99999993	29999999999
29	9999999999999998984	99999993	89999999999
30	9999999999999998984	99999993	89999999999

(S) Fig. 6-- $P_d$  of 3000-m<sup>2</sup> target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

## RADIAL SPEED (KNOTS)

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	99999999995	1477643	37
6	9999999999971	269865	5999
7	9999999999983	1489861	1699999
8	9999999999994	599982	28999999
9	99999999999951	379993	499999999
10	99999999999996	489994	599999999
11	999999999999972	599995	16999999999
12	999999999999998	199996	17999999999
13	9999999999999983	279997	79999999999
14	9999999999999994	279997	38999999999
15	9999999999999999	389998	99999999999
16	99999999999999996	999993	49999999999
17	999999999999999961	999993	99999999999
18	999999999999999991	159994	59999999999
19	999999999999999992	169994	16999999999
20	999999999999999998	699995	19999999999
21	999999999999999998	799996	79999999999
22	9999999999999999983	799996	28999999999
23	9999999999999999994	899996	29999999999
24	9999999999999999994	299997	89999999999
25	99999999999999999951	399997	99999999999
26	99999999999999999991	399998	49999999999
27	99999999999999999992	499998	49999999999
28	99999999999999999992	499998	59999999999
29	99999999999999999992	599999	19999999999
30	99999999999999999992	1599999	19999999999

(S) Fig. 7-- $P_d$  of 3000-m<sup>2</sup> target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

SECRET

NRL REPORT 7765

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99999999961								13321							3
6	99999999982								25421							1599
7	999999999994								147542							279999
8	9999999999981								158754							48999999
9	99999999999971								29865							599999999
10	999999999999982								1379761							16999999999
11	999999999999993								1489871							27999999999
12	9999999999999994								599982							28999999999
13	9999999999999998								299992							39999999999
14	99999999999999991								399993							49999999999
15	99999999999999997								499994							59999999999
16	9999999999999999971								58999							1999999999999
17	9999999999999999992								59999							6999999999999
18	9999999999999999998								199991							1799999999999
19	9999999999999999999								199991							2999999999999
20	99999999999999999994								299991							8999999999999
21	99999999999999999998								299991							3999999999999
22	99999999999999999999								399992							3999999999999
23	99999999999999999999								389992							9999999999999
24	999999999999999999991								99993							4999999999999
25	999999999999999999991								99993							5999999999999
26	999999999999999999997								99994							1599999999999
27	999999999999999999997								199994							1999999999999
28	999999999999999999997								199994							1999999999999
29	999999999999999999998								199995							6999999999999
30	999999999999999999992								199995							7999999999999

(S) Fig. 8-- $P_d$  of 3000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99999999983								11							1
6	9999999999951								21							279
7	99999999999971								1421							48999
8	999999999999983								25421							15999999
9	999999999999994								6532							269999999
10	9999999999999995								14653							3999999999
11	99999999999999991								25854							49999999999
12	999999999999999971								26965							59999999999
13	999999999999999992								7976							1699999999999
14	9999999999999999998								189861							1999999999999
15	99999999999999999994								199971							2799999999999
16	99999999999999999994								25998							8999999999999
17	99999999999999999999								26998							3899999999999
18	99999999999999999995								7999							4999999999999
19	99999999999999999999								7999							9999999999999
20	9999999999999999999971								8999							5999999999999
21	999999999999999999991								8999							1999999999999
22	999999999999999999992								19999							1999999999999
23	999999999999999999998								15999							6999999999999
24	999999999999999999998								69991							1799999999999
25	999999999999999999999								69991							2999999999999
26	9999999999999999999983								79991							2999999999999
27	9999999999999999999994								79991							7999999999999
28	9999999999999999999994								79991							8999999999999
29	9999999999999999999995								89992							3999999999999
30	9999999999999999999999								89992							4999999999999

(S) Fig. 9-- $P_d$  of 3000-m<sup>2</sup> target at 2000-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

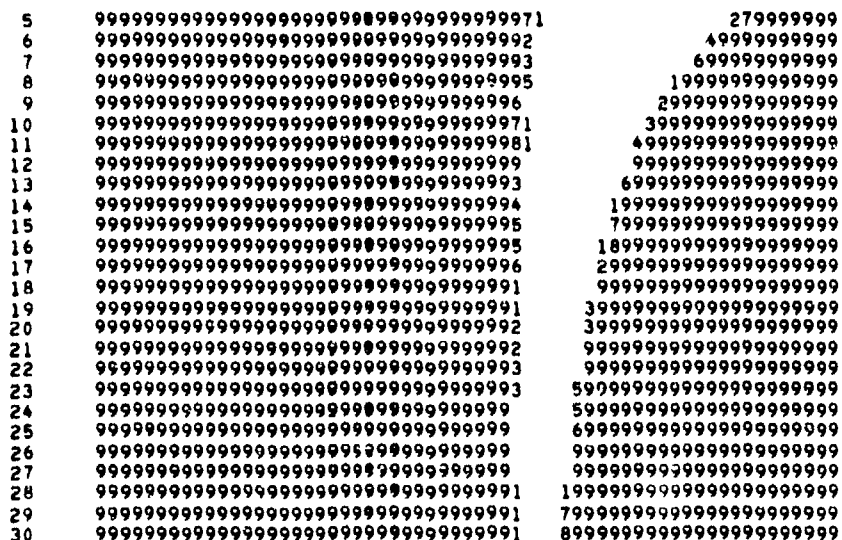
**SECRET**

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30



(S) Fig. 10— $P_d$  of 50,000-m<sup>2</sup> target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30



(S) Fig. 11-- $P_d$  of 50,000-m<sup>2</sup> target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

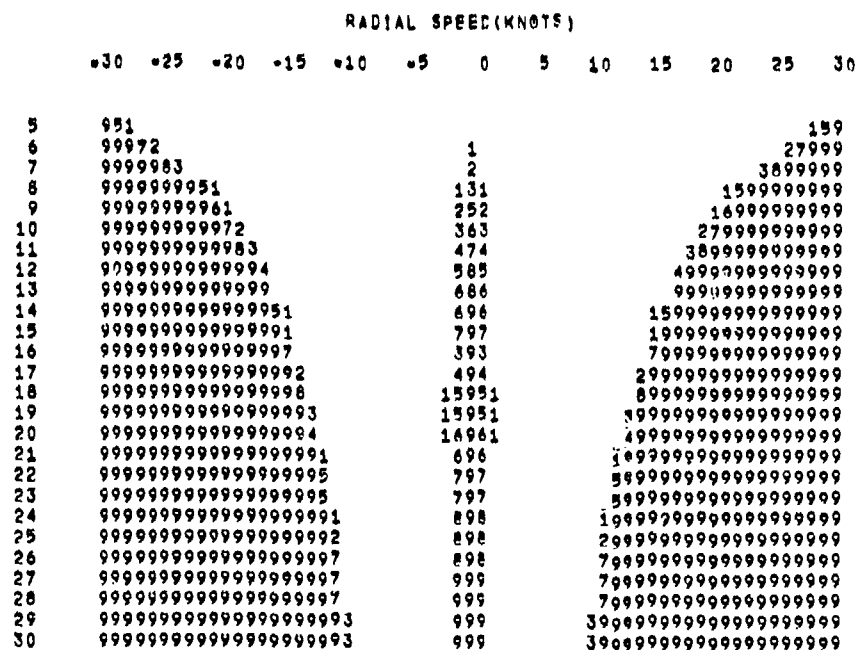
NRL REPORT 7765

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

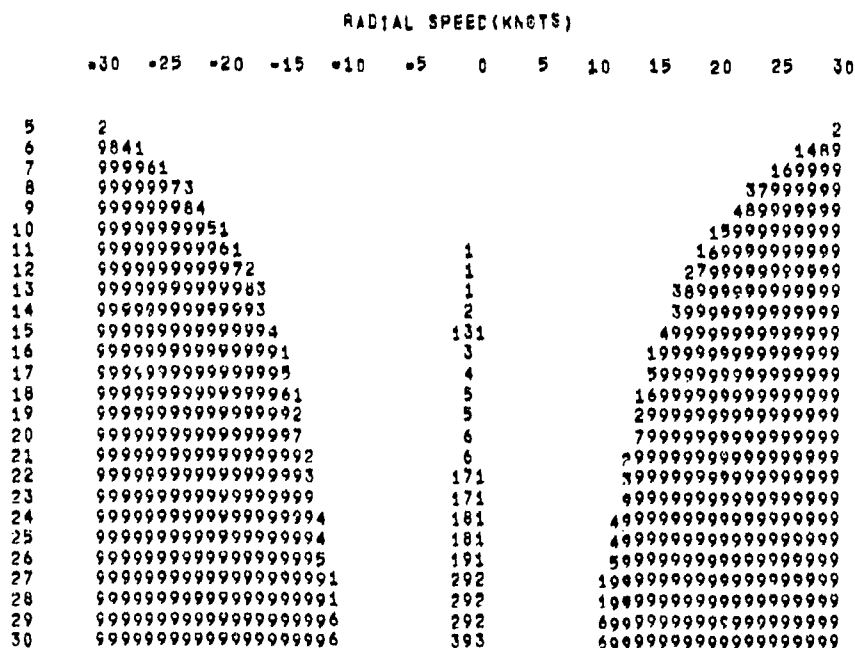
(S) Fig. 12-- $P_d$  of 50,000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -17$  dB

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

(S) Fig. 13  $P_d$  of 50,000-m<sup>2</sup> target at 2000 n.mi. range in approaching sea clutter,  $\sigma_0 = -1.7$  dB



(S) Fig. 14— $P_d$  of a  $1000\text{-m}^2$  target at 500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

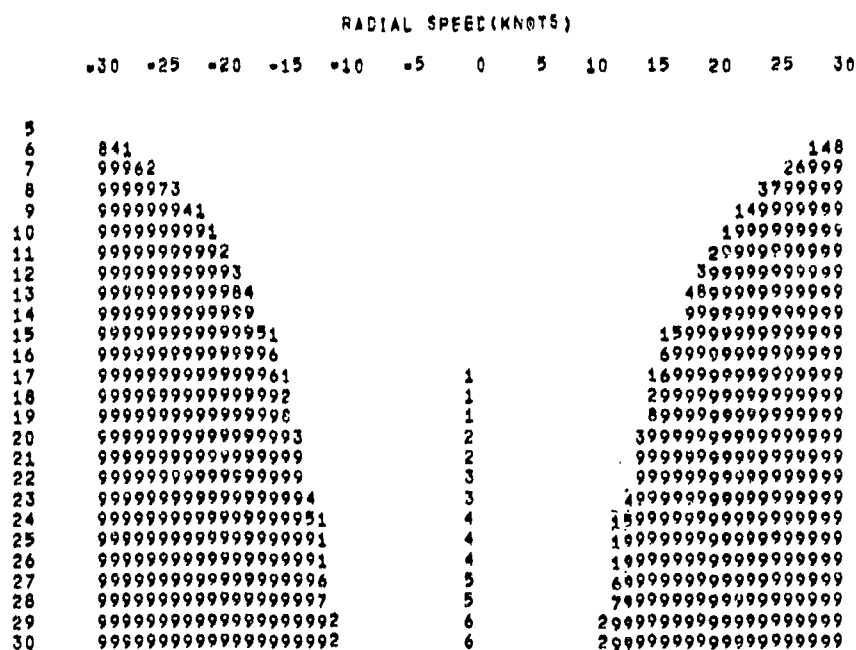


(S) Fig. 15— $P_d$  of a  $1000\text{-m}^2$  target at 1000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

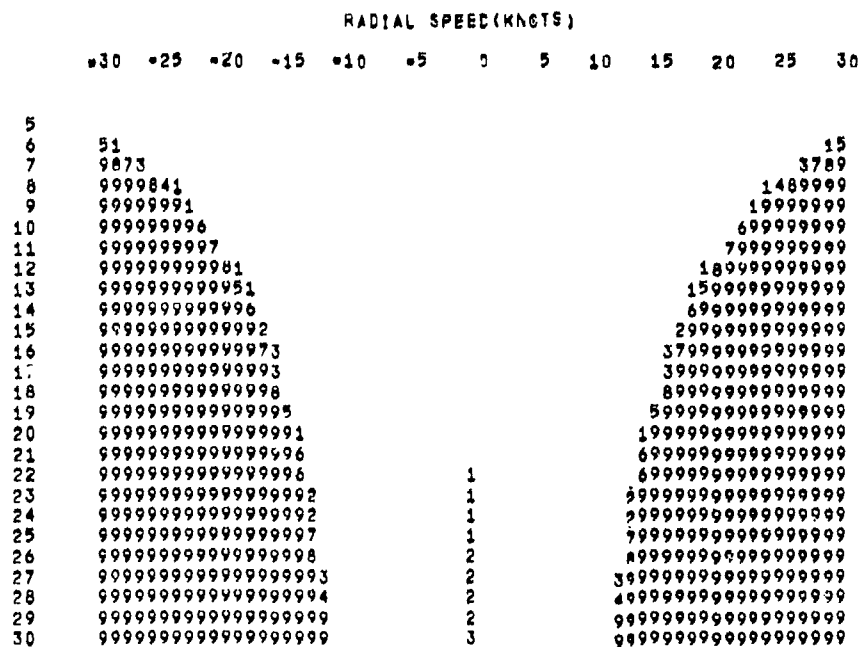


SECRET

NRL REPORT 7765



(S) Fig. 16— $P_d$  of a 1000-m<sup>2</sup> target at 1500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB



(S) Fig. 17— $P_d$  of a 1000-m<sup>2</sup> target at 2000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99961									37973						16999
6	99999883									1599951						38899999
7	9999999951									1699961						1599999999
8	999999999961									3899983						169999999999
9	9999999999972									4999994						279999999999
10	9999999999984									99999						489999999999
11	9999999999991									1699961						199999999999
12	99999999999961									1799971						169999999999
13	99999999999996									1899981						699999999999
14	999999999999992									2999992						299999999999
15	999999999999998									3999993						899999999999
16	9999999999999984									99999						489999999999
17	9999999999999991									99999						199999999999
18	9999999999999995									99999						599999999999
19	9999999999999996									99999						699999999999
20	99999999999999992									99999						299999999999
21	99999999999999992									1699961						299999999999
22	99999999999999997									1799971						799999999999
23	99999999999999998									79997						899999999999
24	999999999999999994									89998						499999999999
25	999999999999999994									89998						499999999999
26	999999999999999999									99999						999999999999
27	999999999999999999									99999						999999999999
28	999999999999999999									99999						999999999999
29	9999999999999999996									99999						699999999999
30	9999999999999999996									99999						699999999999

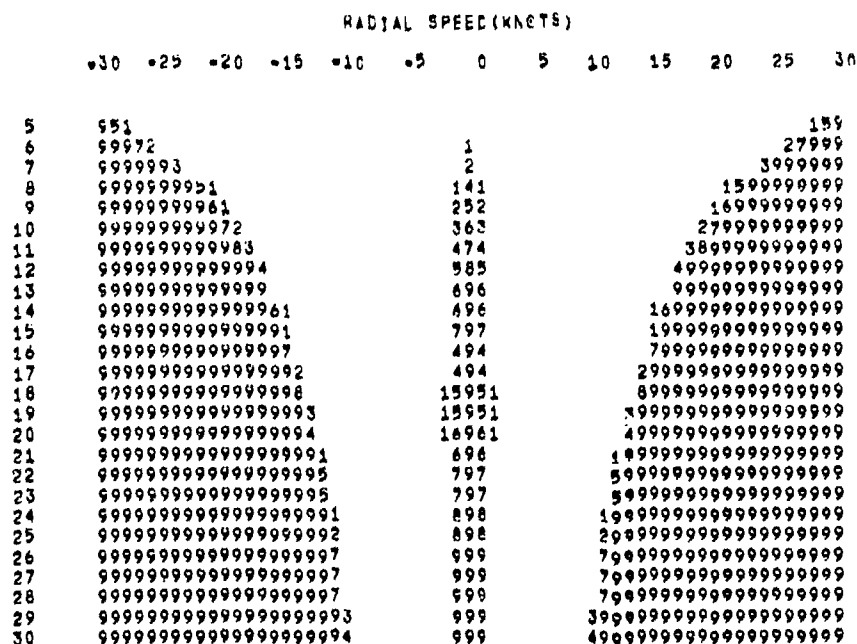
(S) Fig. 18— $P_d$  of a 3000-m<sup>2</sup> target at 500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	994									131						499
6	9999611									252						1169999
7	99999982									363						2899999
8	999999994									15851						499999999
9	999999999951									26962						1599999999
10	9999999999961									37973						1699999999
11	9999999999972									898						2799999999
12	9999999999998									19991						8999999999
13	99999999999994									19991						4999999999
14	999999999999994									19991						4999999999
15	9999999999999951									29992						1599999999
16	9999999999999991									38983						1999999999
17	99999999999999962									38983						3699999999
18	99999999999999992									49994						9999999999
19	999999999999999998									49994						9999999999
20	9999999999999999983									59995						3899999999
21	9999999999999999994									999						4999999999
22	9999999999999999991									999						1999999999
23	9999999999999999991									19991						1999999999
24	9999999999999999995									19991						5999999999
25	9999999999999999996									19991						6999999999
26	9999999999999999992									19991						2999999999
27	9999999999999999992									29992						2999999999
28	9999999999999999992									29992						2999999999
29	9999999999999999997									29992						7999999999
30	9999999999999999998									39993						8999999999

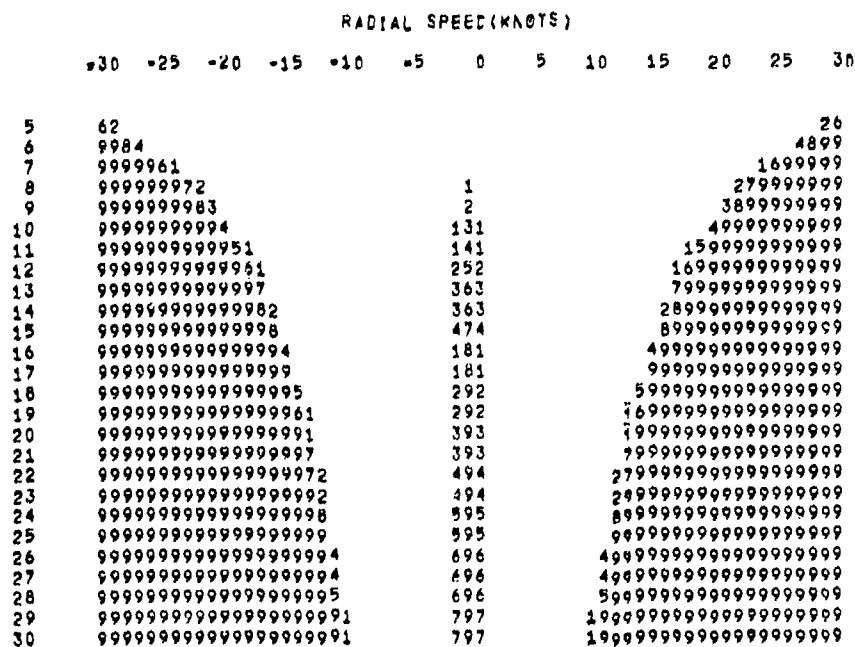
(S) Fig. 19— $P_d$  of a 3000-m<sup>2</sup> target at 1000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

SECRET

NRL REPORT 7765



(S) Fig. 20— $P_d$  of a 3000-m<sup>2</sup> target at 1500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB



(S) Fig. 21— $P_d$  of a 3000-m<sup>2</sup> target at 2000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -17$  dB

## RADIAL SPEED (KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	9999999993						1799999999971					3999999999	
6	9999999995						3999999999993					5999999999	
7	99999999971						5999999999995					1799999999999	
8	999999999981						1699999999961					1899999999999	
9	999999999992						2799999999972					2999999999999	
10	9999999999993						3999999999993					3999999999999	
11	9999999999999						4999999999994					9999999999999	
12	99999999999995						15999999999951					5999999999999	
13	999999999999991						6999999999996					1999999999999	
14	999999999999997						10999999999991					7999999999999	
15	9999999999999982						2999999999992					2899999999999	
16	9999999999999992						38999999999983					2999999999999	
17	9999999999999999						3999999999993					9999999999999	
18	99999999999999994						1999999999991					4999999999999	
19	99999999999999994						1999999999991					4999999999999	
20	99999999999999995						15999999999951					5999999999999	
21	999999999999999951						6999999999996					1999999999999	
22	999999999999999951						6999999999996					1999999999999	
23	999999999999999956						7999999999997					6999999999999	
24	999999999999999957						7999999999997					7999999999999	
25	999999999999999957						3999999999993					7999999999999	
26	9999999999999999592						3999999999993					2999999999999	
27	9999999999999999592						4999999999994					2999999999999	
28	9999999999999999593						4999999999994					3999999999999	
29	9999999999999999593						5999999999995					3999999999999	
30	9999999999999999595						1999999999991					6999999999999	

(S) Fig. 22— $P_d$  of a 50,000- $m^2$  target at 500-n.mi. range in crosswind sea clutter,  $\sigma_0 = -17$  dB

## RADIAL SPEED (KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	9999999993						1799999999971					3999999999	
6	9999999995						2899999999982					5999999999	
7	99999999996						3999999999993					6999999999	
8	9999999999981						9999999999999					1899999999999	
9	9999999999992						1699999999961					2999999999999	
10	99999999999993						1799999999971					3999999999999	
11	999999999999994						8999999999998					4999999999999	
12	999999999999995						3999999999993					9999999999999	
13	9999999999999996						4999999999994					6999999999999	
14	99999999999999971						5999999999995					1799999999999	
15	99999999999999991						6999999999996					1999999999999	
16	99999999999999998						1999999999991					8999999999999	
17	99999999999999992						2999999999992					2999999999999	
18	99999999999999992						2799999999972					2999999999999	
19	99999999999999999						3899999999983					9999999999999	
20	99999999999999999						9999999999999					9999999999999	
21	999999999999999994						9999999999999					4999999999999	
22	999999999999999995						9999999999999					5999999999999	
23	999999999999999995						9999999999999					9999999999999	
24	999999999999999995						1599999999951					9999999999999	
25	9999999999999999951						6999999999996					1999999999999	
26	9999999999999999956						6999999999996					6999999999999	
27	9999999999999999957						6999999999996					7999999999999	
28	9999999999999999957						7999999999997					7999999999999	
29	9999999999999999959						7999999999997					9999999999999	
30	99999999999999999592						7999999999997					2999999999999	

(S) Fig. 23— $P_d$  of a 50,000- $m^2$  target at 1000-n.mi. range in crosswind sea clutter,  $\sigma_0 = -17$  dB

SECRET

NRL REPORT 7765

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999999995															
6	99999999971															
7	999999999982															
8	9999999999994															
9	9999999999995															
10	99999999999996															
11	999999999999971															
12	999999999999991															
13	9999999999999992															
14	9999999999999992															
15	9999999999999999															
16	99999999999999994															
17	99999999999999995															
18	99999999999999999															
19	999999999999999999															
20	999999999999999996															
21	9999999999999999991															
22	99999999999999999991															
23	99999999999999999992															
24	99999999999999999992															
25	99999999999999999999															
26	999999999999999999992															
27	999999999999999999992															
28	999999999999999999993															
29	999999999999999999999															
30	999999999999999999999															

(S) Fig. 24— $P_d$  of a 50,000-m<sup>2</sup> target at 1500-n.mi. range in crosswind sea clutter,  $\sigma_0 = -17$  dB

				RADIAL SPEED (KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999999972															
6	9999999994															
7	99999999996															
8	999999999991															
9	9999999999992															
10	99999999999993															
11	999999999999994															
12	999999999999999															
13	9999999999999996															
14	99999999999999991															
15	99999999999999997															
16	999999999999999981															
17	999999999999999992															
18	999999999999999999															
19	9999999999999999993															
20	9999999999999999993															
21	9999999999999999999															
22	9999999999999999999															
23	99999999999999999995															
24	99999999999999999995															
25	99999999999999999996															
26	99999999999999999999															
27	99999999999999999999															
28	999999999999999999991															
29	999999999999999999997															
30	999999999999999999998															

(S) Fig. 25— $P_d$  of a 50,000-m<sup>2</sup> target at 2000-n.mi. range in crosswind sea clutter,  $\sigma_0 = -17$  dB

## RADIAL SPEED (KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99999999999994					27999999971							2899
6	999999999999961					4899999993						4499999	
7	999999999999971					1599999994						169999999	
8	999999999999993					1799999996						27999999999	
9	9999999999999941					28999999971						38999999999	
10	9999999999999951					4999999998						49999999999	
11	9999999999999961					5999999993						5999999999999	
12	999999999999997311					6999999994						1999999999999	
13	999999999999998216					9999999995						2799999999999	
14	999999999999999312					9999999995						8999999999999	
15	999999999999999622					9999999996						4899999999999	
16	999999999999999864					3899999997						1499999999999	
17	999999999999999905					4999999997						5999999999999	
18	999999999999999906					4999999998						1699999999999	
19	999999999999999908					4999999998						2999999999999	
20	99999999999999990856					9999999999						7999999999999	
21	99999999999999990976					9999999993						7999999999999	
22	99999999999999990987					9999999993						3999999999999	
23	9999999999999999098799					9999999994						3999999999999	
24	999999999999999909879999					9999999994						8999999999999	
25	9999999999999999099799					9999999995						1999999999999	
26	999999999999999909979999					9999999995						5999999999999	
27	9999999999999999099899					9999999995						5999999999999	
28	999999999999999909989999					9999999996						6999999999999	
29	999999999999999909989999					9999999996						1999999999999	
30	999999999999999909989999					9999999996						2999999999999	

(S) Fig. 26— $P_d$  of a 1000-m<sup>2</sup> target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

## RADIAL SPEED (KNOTS)

	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999999999999822					137999761							169
6	999999999999994					25999982							28999
7	9999999999999961					37999993							4999999
8	9999999999999971					8999995						159999999	
9	9999999999999982					16999961						17999999999	
10	9999999999999999					27999971						28999999999	
11	9999999999999995					8999998						39999999999	
12	99999999999999991					4999999						4999999999999	
13	99999999999999996					5999999						1999999999999	
14	999999999999999972					5999999						1699999999999	
15	999999999999999992					6999999						1999999999999	
16	999999999999999999					1999996						7999999999999	
17	9999999999999999993					29999961						2999999999999	
18	9999999999999999994					28999971						8999999999999	
19	99999999999999999951					38999971						4999999999999	
20	99999999999999999991					9999982						4999999999999	
21	999999999999999999921					999998						1999999999999	
22	999999999999999999961					999999						5999999999999	
23	999999999999999999971					1999999						6999999999999	
24	9999999999999999999711					1699999						1999999999999	
25	9999999999999999999741					1699999						2999999999999	
26	9999999999999999999841					1699999						7999999999999	
27	9999999999999999999941					1799999						7999999999999	
28	9999999999999999999991					1799999						8999999999999	
29	99999999999999999999951					1899999						3999999999999	
30	999999999999999999999848					9999999						4999999999999	

(S) Fig. 27— $P_d$  of a 1000-m<sup>2</sup> target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

SECRET

## NRL REPORT 7765

		RADIAL SPEED(KNOTS)												
		-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99999999994							366532						26
6	999999999961							158754						4899
7	9999999999972							379875					1599999	
8	449999499999993							4899871					179999999	
9	999999999999994							2599982					289999999	
10	999999999999995							3899993					399999999	
11	9999999999999961							4799994					599999999	
12	999999999999997							8999995					159999999	
13	9999999999999982							1599995					699999999	
14	9999999999999993							1699996					279999999	
15	9999999999999999							2799997					899999999	
16	9999999999999994							8999992					399999999	
17	9999999999999995							8999992					999999999	
18	99999999999999991							4999993					499999999	
19	99999999999999997							5999994					599999999	
20	99999999999999997							5999994					199999999	
21	99999999999999982							6999995					699999999	
22	99999999999999992							6999995					169999999	
23	99999999999999993							1999996					299999999	
24	99999999999999993							2999996					799999999	
25	99999999999999991							2999997					899999999	
26	99999999999999991							2999997					389999999	
27	99999999999999991							3999997					399999999	
28	99999999999999991							3999997					399999999	
29	99999999999999995							4999998					999999999	
30	99999999999999995							4999998					999999999	

(S) Fig. 28— $P_d$  of a 1000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

		RADIAL SPEED(KNOTS)												
		-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999999999961							13321						3
6	9999999999983							25421						1599
7	9999999999994							147542						279999
8	99999999999961							158754						4899999
9	99999999999971							29865					5999999	
10	99999999999982							1379761					169999999	
11	99999999999993							1589871					279999999	
12	999999999999994							599982					289999999	
13	999999999999995							299992					399999999	
14	9999999999999991							399993					499999999	
15	9999999999999997							499994					599999999	
16	99999999999999972							58999					199999999	
17	9999999999999992							59999					699999999	
18	99999999999999988							199991					179999999	
19	99999999999999999							199991					299999999	
20	99999999999999994							299991					899999999	
21	99999999999999994							299991					399999999	
22	99999999999999995							399992					399999999	
23	99999999999999999							389992					999999999	
24	99999999999999991							99993					499999999	
25	99999999999999991							99993					599999999	
26	99999999999999997							99994					159999999	
27	99999999999999997							199994					199999999	
28	99999999999999997							199994					199999999	
29	99999999999999998							199995					699999999	
30	99999999999999992							199995					799999999	

(S) Fig. 29— $P_d$  of a 1000-m<sup>2</sup> target at 2000-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

SECRET

**SECRET**

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

[illegible]

(S) Fig. 30— $P_d$  of a 3000-m<sup>2</sup> target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	999999999999999982	1699999999995	17999
6	9999999999999999041	2289999999997	38899999
7	99999999999999990621	4999999999982	159999999
8	99999999999999990731	1699999999994	16999999999
9	99999999999999990841	1278999999995	27999999999
10	99999999999999990951	2889999999999	48999999999
11	99999999999999991061	3389999999971	19999999999
12	99999999999999991171	4499999999981	16999999999
13	99999999999999991281	5499999999992	69999999999
14	99999999999999991391	6599999999993	29999999999
15	99999999999999991501	7699999999993	89999999999
16	99999999999999991611	8799999999999	49999999999
17	99999999999999991721	9899999999999	19999999999
18	99999999999999991831	1099999999999	59999999999
19	99999999999999991941	2199999999999	69999999999
20	99999999999999992051	3299999999999	29999999999
21	99999999999999992161	4399999999999	29999999999
22	99999999999999992271	5499999999999	79999999999
23	99999999999999992381	6599999999999	89999999999
24	99999999999999992491	7699999999999	49999999999
25	99999999999999992601	8799999999999	49999999999
26	99999999999999992711	9899999999999	99999999999
27	99999999999999992821	1099999999999	99999999999
28	99999999999999992931	2199999999999	99999999999
29	99999999999999993041	3299999999999	69999999999
30	99999999999999993151	4399999999999	69999999999

(S) Fig. 31— $P_d$  of a 3000-m<sup>2</sup> target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

**SECRET**



NRL REPORT 7765

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

[illegible]

(S) Fig. 32— $P_d$  of a 3000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	999999999999771	489099994	599
6	99999999999983	169999961	1179999
7	99999999999984	2790999081	38999999
8	999999999999861	499999993	4999999999
9	99999999999993971	1599999994	169999999999
10	9999999999999902	1699999995	179999999999
11	99999999999999903	299999991	289999999999
12	999999999999999941	399999991	89999999999999
13	9999999999999999991	399999992	49999999999999
14	99999999999999999961	999999992	5999999999999999
15	99999999999999999973	199999993	1699999999999999
16	999999999999999999921	169999994	2999999999999999
17	999999999999999999982	169999995	2799999999999999
18	999999999999999999983	179999995	3999999999999999
19	999999999999999999985	179999996	8999999999999999
20	999999999999999999986	299999996	4899999999999999
21	9999999999999999999864	399999991	4999999999999999
22	999999999999999999989	499999991	1999999999999999
23	9999999999999999999895	499999991	1999999999999999
24	9999999999999999999895	599999991	6999999999999999
25	9999999999999999999898	999999992	6999999999999999
26	99999999999999999998985	999999992	2999999999999999
27	99999999999999999998985	999999992	2999999999999999
28	99999999999999999998985	999999993	3999999999999999
29	999999999999999999989899	999999993	8999999999999999
30	999999999999999999989899	999999994	8999999999999999

(S) Fig. 33— $P_d$  of a 3000-m<sup>2</sup> target at 2000-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

**SECRET**

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

[illegible]

(S) Fig. 34— $P_d$  of a 50,000-m<sup>2</sup> target at 500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

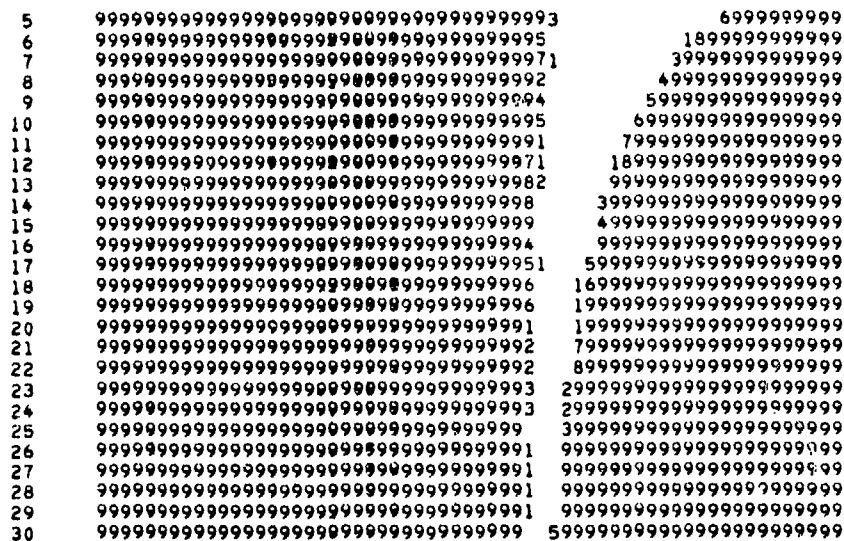
[illegible]

(S) Fig. 35— $P_d$  of a 50,000-m<sup>2</sup> target at 1000-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

**SECRET**

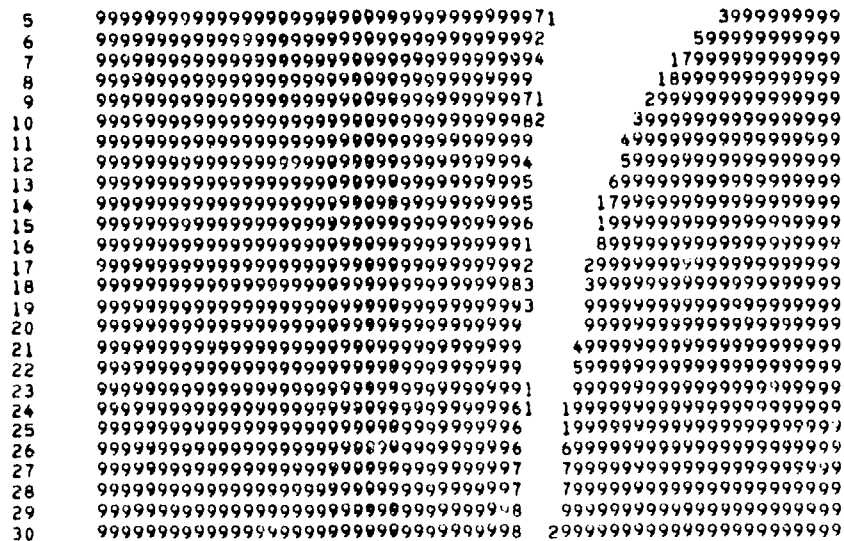
NRL REPORT 7765

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

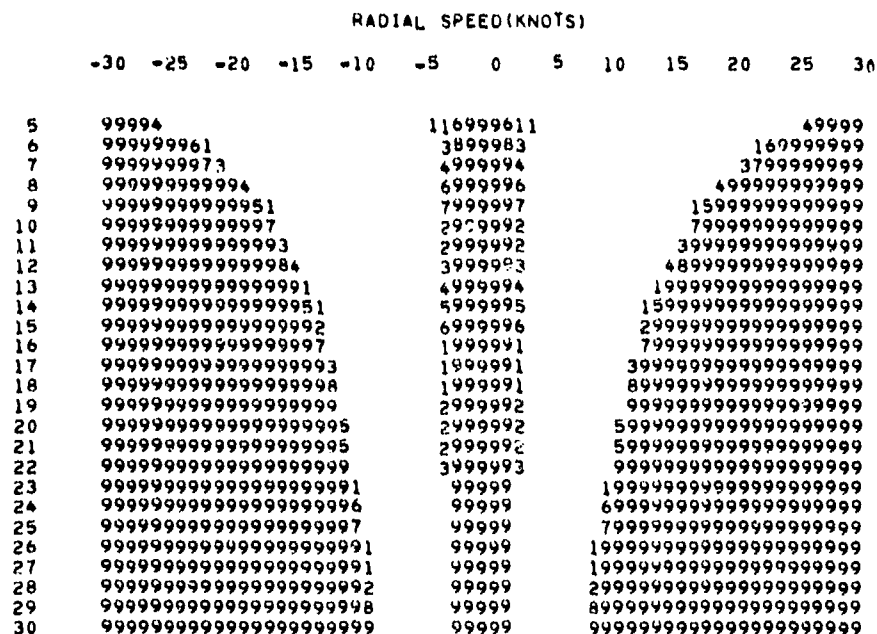


(S) Fig. 36— $P_d$  of a 50,000-m<sup>2</sup> target at 1500-n.mi. range in approaching sea clutter,  $\sigma_0 = -23$  dB

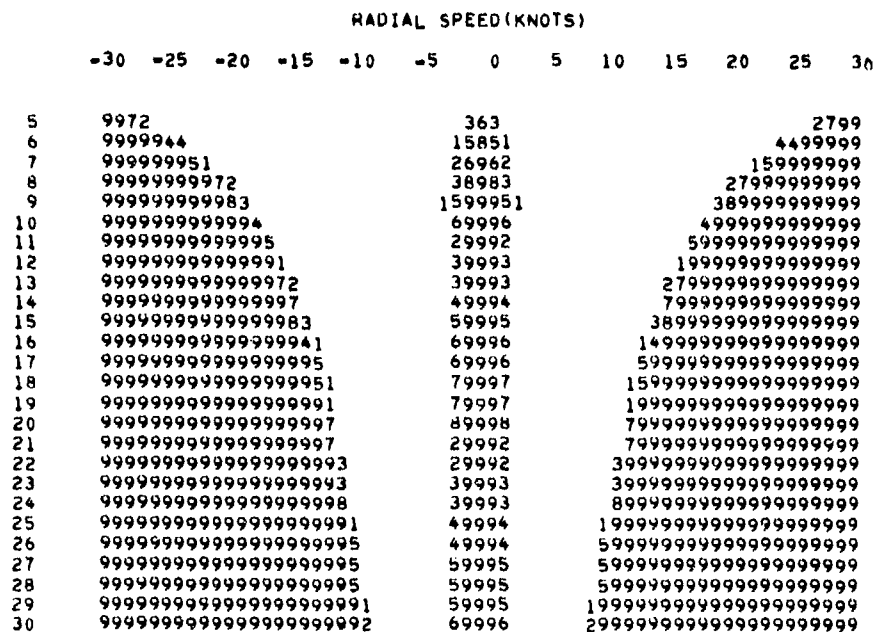
-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30



(S) Fig. 37  $-P_d$  of a 50,000-m<sup>2</sup> target at 2000-n.mi. range in approaching sea clutter,  $\theta_0 = -23$  dB



(S) Fig. 38— $P_d$  of a 1000-m<sup>2</sup> target at 500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB



(S) Fig. 39— $P_d$  of a 1000-m<sup>2</sup> target at 1000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB

SECRET

NRL REPORT 7765

RADIAL SPEED (KNOTS)													
	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	983						2						389
6	9999511						141					1159999	
7	99999971						252					17999999	
8	999999983						474					389999999	
9	9999999994						15851					4999999999	
10	999999999951						26962				159999999999		
11	9999999999961						797				1699999999999		
12	9999999999997						898				7999999999999		
13	99999999999992						999				29999999999999		
14	999999999999983						19991				389999999999999		
15	999999999999994						19991				499999999999999		
16	9999999999999991						27972				1999999999999999		
17	99999999999999951						27972				15999999999999999		
18	99999999999999991						38983				19999999999999999		
19	99999999999999996						38983				69999999999999999		
20	999999999999999972						49994				27999999999999999		
21	999999999999999993						999				39999999999999999		
22	999999999999999998						999				89999999999999999		
23	999999999999999998						999				89999999999999999		
24	9999999999999999994						999				49999999999999999		
25	9999999999999999998						19991				59999999999999999		
26	99999999999999999901						19991				19999999999999999		
27	99999999999999999901						19991				19999999999999999		
28	99999999999999999901						19991				19999999999999999		
29	99999999999999999906						19991				69999999999999999		
30	99999999999999999907						29992				79999999999999999		

(S) Fig. 40— $P_d$  of a 1000-m<sup>2</sup> target at 1500-n.mi. range in crosswind sea clutter,  $\sigma_0 = -23$  dB

RADIAL SPEED(KNOTS)													
	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	951												159
6	99972						1						27999
7	9999994						2						4999999
8	9999999951						141						1599999999
9	99999999961						252						16999999999
10	999999999972						363						279999999999
11	9999999999983						474						3899999999999
12	9999999999994						585						4999999999999
13	9999999999999						696						9999999999999
14	999999999999961						696						169999999999999
15	999999999999991						797						199999999999999
16	999999999999997						494						799999999999999
17	9999999999999992						494						299999999999999
18	9999999999999998						15951						899999999999999
19	99999999999999993						15951						399999999999999
20	99999999999999994						16961						499999999999999
21	99999999999999991						696						199999999999999
22	99999999999999995						797						599999999999999
23	99999999999999996						797						699999999999999
24	99999999999999991						898						199999999999999
25	99999999999999992						898						299999999999999
26	99999999999999997						999						799999999999999
27	99999999999999997						999						799999999999999
28	99999999999999998						999						899999999999999
29	99999999999999993						999						399999999999999
30	99999999999999994						999						499999999999999

(S) Fig. 41— $P_d$  of a 1000-m<sup>2</sup> target at 2000-n.mi. range in crosswind sea clutter,  $\sigma_0 = -23$  dB

JON DAVID WILSON

SECRET

				RADIAL SPEED(KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	999999962		6999999996												269999999	
6	9999999983		1899999981												3899999999	
7	99999999995		2999999992												5999999999	
8	9999999999991		4999999994												199999999999	
9	99999999999991		599999995												19999999999999	
10	99999999999992		699999996												29999999999999	
11	99999999999993		1799999971												39999999999999	
12	99999999999999		899999998												99999999999999	
13	999999999999995		299999992												59999999999999	
14	999999999999999		399999993												99999999999999	
15	999999999999997		499999994												79999999999999	
16	9999999999999971		499999994												17999999999999	
17	9999999999999991		599999995												19999999999999	
18	9999999999999999		199999991												99999999999999	
19	9999999999999992		199999991												29999999999999	
20	9999999999999993		199999991												39999999999999	
21	9999999999999999		299999992												99999999999999	
22	9999999999999999		299999992												99999999999999	
23	9999999999999994		289999982												49999999999999	
24	9999999999999995		9999999												59999999999999	
25	9999999999999999		9999999												59999999999999	
26	9999999999999999		9999999												99999999999999	
27	9999999999999999		9999999												99999999999999	
28	9999999999999999		9999999												99999999999999	
29	9999999999999997		9999999												79999999999999	
30	9999999999999997		199999991												79999999999999	

(S) Fig. 42— $P_c$  of a 3000-m<sup>2</sup> target at 500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB

				RADIAL SPEED(KNOTS)												
				-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	9999833		559999955												3389999	
6	999999951		179999971												159999999	
7	9999999972		289999982												2799999999	
8	99999999984		399999993												489999999999	
9	999999999995		9999999												59999999999999	
10	9999999999992		6999996												29999999999999	
11	99999999999972		179999971												27999999999999	
12	99999999999983		189999981												38999999999999	
13	99999999999994		8999998												49999999999999	
14	999999999999995		9999999												59999999999999	
15	999999999999996		9999999												69999999999999	
16	9999999999999991		4999994												19999999999999	
17	9999999999999997		5999995												79999999999999	
18	9999999999999991		5999995												19999999999999	
19	9999999999999992		6999996												29999999999999	
20	9999999999999999		6999996												99999999999999	
21	9999999999999993		7999997												39999999999999	
22	9999999999999994		7999997												39999999999999	
23	9999999999999999		1999991												49999999999999	
24	9999999999999999		1999991												99999999999999	
25	9999999999999999		2999992												99999999999999	
26	9999999999999995		2999992												59999999999999	
27	9999999999999996		2999992												69999999999999	
28	9999999999999996		3999993												69999999999999	
29	9999999999999999		3999993												99999999999999	
30	9999999999999991		4999994												19999999999999	

(S) Fig. 43— $P_d$  of a 3000-m<sup>2</sup> target at 1000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB

SECRET

SECRET

NRL REPORT 7765

RADIAL SPEED(KNOTS)													
	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99994						116999611					49999	
6	999999961						3899983					169999999	
7	9999999973						4999994					379999999	
8	999999999941						6999996					14999999999	
9	9999999999951						7999997					1599999999999	
10	9999999999997						2499992					7999999999999	
11	99999999999993						2999992					3999999999999	
12	999999999999984						3999993					4899999999999	
13	999999999999991						4999994					1999999999999	
14	9999999999999951						5999995					1599999999999	
15	9999999999999992						6999996					2999999999999	
16	9999999999999997						1999991					7999999999999	
17	9999999999999993						1999991					3499999999999	
18	9999999999999998						1999991					8999999999999	
19	9999999999999999						2999992					9999999999999	
20	9999999999999995						2999992					5999999999999	
21	9999999999999995						2999992					5999999999999	
22	9999999999999999						3999993					9999999999999	
23	99999999999999991						99999					1999999999999	
24	99999999999999997						99999					7999999999999	
25	99999999999999997						99999					7999999999999	
26	99999999999999991						99999					1999999999999	
27	99999999999999992						99999					2999999999999	
28	99999999999999992						99999					2999999999999	
29	99999999999999998						99999					8999999999999	
30	99999999999999999						99999					9999999999999	

(S) Fig. 44-- $P_d$  of a 3000-m<sup>2</sup> target at 1500-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB

RADIAL SPEED(KNOTS)													
	-30	-25	-20	-15	-10	-5	0	5	10	15	20	25	30
5	99961						37973					16999	
6	99999883						1599951					38899999	
7	9999999941						1699961					1499999999	
8	999999999961						3899983					1699999999	
9	999999999972						4999994					279999999999	
10	9999999999983						99999					38999999999999	
11	99999999999991						69996					19999999999999	
12	999999999999951						1799971					1599999999999999	
13	999999999999996						1899981					6999999999999999	
14	9999999999999992						2899982					2999999999999999	
15	9999999999999998						3999993					8999999999999999	
16	9999999999999984						99999					4899999999999999	
17	9999999999999991						99999					199999999999999999	
18	9999999999999995						99999					599999999999999999	
19	9999999999999996						99999					699999999999999999	
20	9999999999999992						99999					299999999999999999	
21	9999999999999992						69996					299999999999999999	
22	9999999999999997						1799971					799999999999999999	
23	9999999999999998						79997					899999999999999999	
24	9999999999999993						89998					399999999999999999	
25	9999999999999994						89998					499999999999999999	
26	9999999999999995						89998					999999999999999999	
27	9999999999999995						99999					999999999999999999	
28	9999999999999995						99999					999999999999999999	
29	9999999999999995						99999					599999999999999999	
30	9999999999999996						99999					699999999999999999	

(S) Fig. 45-- $P_d$  of a 3000-m<sup>2</sup> target at 2000-n.mi. range in crosswind  
sea clutter,  $\sigma_0 = -23$  dB





SECRET

NRL REPORT 7765

RADIAL SPEED(KNOTS)

-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	9999999996	4999999999999994	6999999999
6	999999999981	116999999999999611	189999999999
7	9999999999993	2899999999999982	399999999999
8	99999999999994	49999999999994	49999999999999
9	999999999999996	1599999999999951	69999999999999
10	9999999999999971	69999999999996	17999999999999
11	9999999999999992	279999999999972	29999999999999
12	9999999999999982	389999999999983	28999999999999
13	9999999999999993	999999999999	39999999999999
14	9999999999999999	149999999999941	99999999999999
15	99999999999999995	159999999999951	59999999999999
16	999999999999999961	69999999999996	16999999999999
17	999999999999999991	69999999999996	19999999999999
18	999999999999999997	39999999999993	79999999999999
19	999999999999999997	39999999999993	79999999999999
20	999999999999999982	48999999999984	28999999999999
21	999999999999999993	19999999999991	39999999999999
22	999999999999999993	19999999999991	39999999999999
23	999999999999999999	29999999999992	99999999999999
24	999999999999999999	29999999999992	99999999999999
25	999999999999999999	69999999996	99999999999999
26	9999999999999999995	79999999997	59999999999999
27	9999999999999999996	79999999997	69999999999999
28	99999999999999999961	799999999971	69999999999999
29	99999999999999999961	899999999981	69999999999999
30	99999999999999999991	149999999994	19999999999999

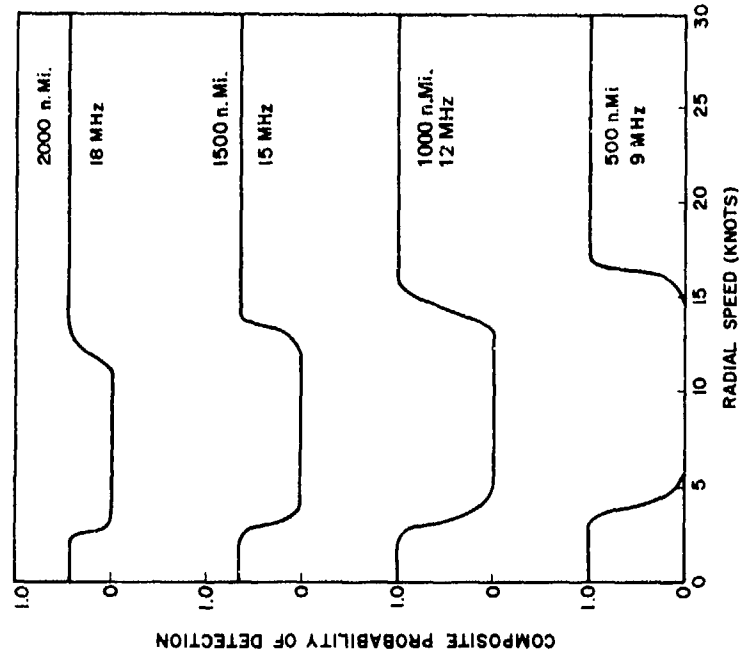
(S) Fig. 48— $P_d$  of a 50,000-m<sup>2</sup> target at 1500-n.mi. range in crosswind sea clutter,  $\sigma_0 = -23$  dB

RADIAL SPEED(KNOTS)

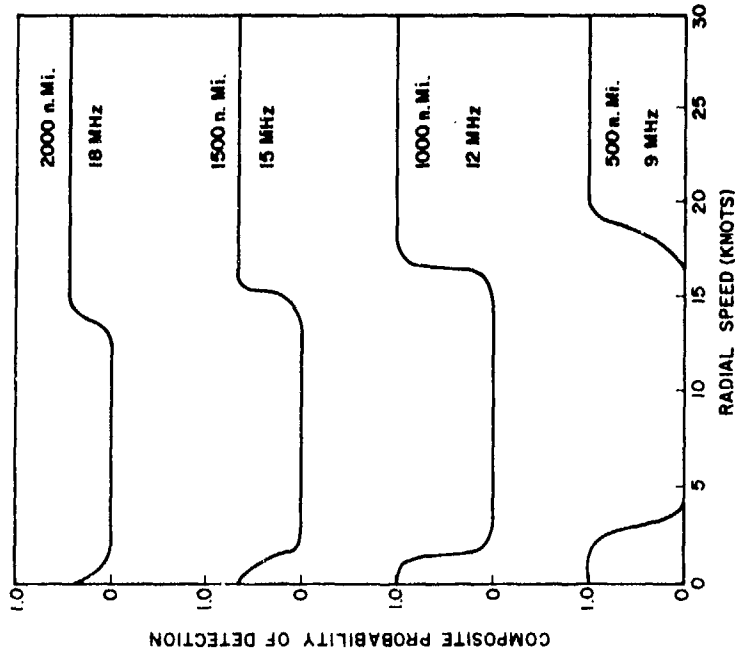
-30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30

5	9999999993	279999999999972	3999999999
6	999999999995	39999999999993	599999999999
7	99999999999971	159999999999951	179999999999
8	99999999999981	169999999999961	189999999999
9	99999999999992	289999999999982	299999999999
10	999999999999994	39999999999993	499999999999
11	9999999999999999	49999999999994	999999999999
12	99999999999999961	159999999999951	169999999999
13	99999999999999991	69999999999996	199999999999
14	99999999999999997	29999999999992	799999999999
15	999999999999999982	29999999999992	289999999999
16	999999999999999992	389999999999983	299999999999
17	999999999999999999	39999999999993	999999999999
18	999999999999999994	14999999999991	499999999999
19	9999999999999999994	14999999999991	499999999999
20	9999999999999999995	159999999999951	599999999999
21	99999999999999999991	69999999999996	199999999999
22	99999999999999999991	69999999999996	199999999999
23	99999999999999999996	79999999999997	699999999999
24	99999999999999999997	79999999999997	799999999999
25	99999999999999999997	39999999999993	799999999999
26	99999999999999999992	49999999999994	299999999999
27	99999999999999999993	49999999999994	399999999999
28	99999999999999999993	49999999999994	399999999999
29	99999999999999999993	59999999999995	399999999999
30	99999999999999999999	19999999999991	999999999999

(S) Fig. 49— $P_d$  of a 50,000-m<sup>2</sup> target at 2000-n.mi. range in crosswind sea clutter,  $\sigma_0 = -23$  dB



(S) Fig. 51—Composite  $P_d$  of a  $3000\text{-m}^2$  target in crosswind sea clutter,  $\sigma_0 = -23\text{ dB}$



(S) Fig. 50—Composite  $P_d$  of a  $3000\text{-m}^2$  target in crosswind sea clutter,  $\sigma_0 = -17\text{ dB}$

below 13 knots if  $\sigma_0 = -23$  dB. The composite  $P_d$ 's are limited at long ranges by the probability of propagation. Thus, the composite  $P_d$  would be raised by any feature which improves propagation, such as allowing multiple-bounce propagation or increasing power.

### ACKNOWLEDGMENTS

(U) I would like to thank Dr. G. V. Trunk for his assistance in formulating the criteria for propagation, and Dr. J. R. Barnum for the advanced copy of sea clutter data and his helpful remarks concerning the nature of sea clutter.

### REFERENCES

1. H.L. Stalford, "A Minimum-Distance Method for Ocean Surveillance Resolution," NRL Report 7677, Mar. 22, 1974.
2. H.L. Stalford, "A Combinatorial Occupancy Method for Determining Parameter Resolution in a Multi-Target Environment," NRL Report 7702, May 1, 1974.
3. H.L. Stalford, "Solitary Occupancy for Unequal Cell Probabilities with Application to Doppler Radars for Ocean Surveillance," NRL Report 7708, May 20, 1974.
4. H.L. Stalford, "Probability That  $N$  ships in an Ocean Surveillance Range-Azimuth Cell Occupy Separate Doppler Bins," NRL Report 7715, May 22, 1974.
5. H.L. Stalford, "Probability of Resolving  $N$  Ships From Radar Observations," NRL Report 7726, May 23, 1974.
6. W.B. Gordon, "Cost Analysis of an OTH Radar System," NRL Report 7752, pending publication.
7. J.M. Headrick, J.F. Thomason, D.L. Lucas, S.R. McCammon, R.A. Hanson, and J.L. Lloyd, "Virtual Path Tracing for HF Radar Including an Ionospheric Model," NRL Memorandum Report 2226, Mar. 29, 1971.
8. W.L. Rubin and J.V. Difrancio, "Radar Detection," *Electro-Tech., Sci. Eng. Ser.* 64, 61-91 (Apr. 1964).
9. J.R. Barnum, "Assorted Sea-Clutter and Single-Signal Spectra Contents and Notes," Stanford Research Institute, Oct. 17, 1973.
10. A.E. Long and D.B. Trizna, "Mapping of North Atlantic Winds by HF Radar Sea Backscatter Interpretation," *IEEE Trans. Antennas and Propagation*, AP-21 (No. 5), (Sept. 1973).
11. M.I. Skolnik, editor, *Radar Handbook*, McGraw-Hill, New York, 1970, Chap. 26.
12. J.R. Barnum, "Ship Ahoy Through March 1973," *Proceedings of the OHD Technical Review Meeting* of May 2-3, 1973, Vol 1, Detection Results, Equipment and Techniques, p. 57-90.

**Naval Research Laboratory  
Technical Library  
Research Reports Section**

**DATE:** July 1, 2002  
**FROM:** Mary Templeman, Code 5227  
**TO:** Code 5300 Paul Hughes  
**CC:** Tina Smallwood, Code 1221.1 *8/21/02*  
**SUBJ:** Review of NRL Reports

Dear Sir/Madam:

Please review NRL Reports ~~7583, 7631~~, 7752, 7765, and MR-3079 for:

- ☒ Possible Distribution Statement  
☐ Possible Change in Classification

Thank you,

*Mary Templeman*

Mary Templeman  
(202)767-3425

[maryt@library.nrl.navy.mil](mailto:maryt@library.nrl.navy.mil)

The subject report can be:

- ☒ Changed to Distribution A (Unlimited) *for Reports 3079, 7765, and 7752*  
☐ Changed to Classification \_\_\_\_\_  
☒ Other: *Reports 7583 AND 7631 should retain their limited distribution statements*

*Paul K. Hughes Jr* *8/21/2002*  
Signature Date

-- 1 OF 1  
-- 1 - AD NUMBER: 531281  
-- 2 - FIELDS AND GROUPS: 15/4, 17/9  
-- 5 - CORPORATE AUTHOR: NAVAL RESEARCH LAB WASHINGTON D C  
-- 6 - UNCLASSIFIED TITLE: PROBABILITY OF DETECTING SHIPS WITH AN OTH  
-- RADAR SYSTEM.  
-- 9 - DESCRIPTIVE NOTE: INTERIM REPT.,  
--10 - PERSONAL AUTHORS: WILSON, JON DAVID ;  
--11 - REPORT DATE: 10 JUL 1974  
--12 - PAGINATION: 48P MEDIA COST: \$ 7.00 PRICE CODE: AA  
--14 - REPORT NUMBER: NRL-7765  
--16 - PROJECT NUMBER: NRL-R02-46A, WF12-111  
--17 - TASK NUMBER: WF12-111-704  
--20 - REPORT CLASSIFICATION: UNCLASSIFIED  
--22 - LIMITATIONS (ALPHA): DISTRIBUTION LIMITED TO U.S. GOV'T.  
-- AGENCIES ONLY; TEST AND EVALUATION; JUL 74. OTHER REQUESTS FOR  
-- THIS DOCUMENT MUST BE REFERRED TO DIRECTOR, NAVAL RESEARCH LAB.,  
-- WASHINGTON, D. C. 20375.  
--23 - DESCRIPTORS: (\*OVER THE HORIZON DETECTION, \*RADAR), (\*SHIPS,  
-- OVER THE HORIZON DETECTION), PROBABILITY, OCEAN SURVEILLANCE, SEA  
-- CLUTTER, IONOSPHERIC PROPAGATION, COMPUTER PROGRAMS, COST  
-- EFFECTIVENESS, RADAR SIGNALS, PROPAGATION, RADAR EQUIPMENT,  
-- SPACEBORNE, AIRBORNE, GROUND STATIONS, TARGET ACQUISITION,  
--  
-- DETECTION  
--24 - DESCRIPTOR CLASSIFICATION: UNCLASSIFIED  
--25 - IDENTIFIERS: RADARC COMPUTER PROGRAMS  
--26 - IDENTIFIER CLASSIFICATION: UNCLASSIFIED

APPROVED FOR PUBLIC  
RELEASE - DISTRIBUTION  
UNLIMITED